UTILIZATION OF BASALT FIBERS AS A RAW MATERIAL FOR CLAY CERAMIC PRODUCTION

SUPAWAN VICHAPHUND, KRITKAEW SOMTON, THASSANEE WONGLOM, MANA RODCHOM, *DUANGDUEN ATONG

Ceramic Technology Research Unit, National Metal and Materials Technology Center, Pathumthani, 12120, Thailand

*E-mail: duangdua@mtec.or.th

Submitted September 14, 2015; accepted January 22, 2016

Keywords: Basalt fiber, Clay-based ceramics, Density, Strength, Stoneware tile

This research aimed to investigate the possibility of utilization basalt fibers as a raw material for ceramic production. Both quartz and feldspar were replaced partially or entirely by basalt fiber in the range of 10 - 25 wt. %. The mixture of ceramic powders and basalt fibers were uniaxially pressed and sintered at temperatures between 1000 and 1200°C for 1 h. The substitution of basalt fibers in ceramic compositions demonstrated the positive effect on the physical and mechanical properties. The addition of basalt fibers in an appropriate amount enhanced the densification and reduced sintering temperature of clay-based ceramics (CB-0) from 1200 to 1150°C. The highest density and strength were 2.40 g cm⁻³ and 116 MPa, respectively, when replacing feldspar and quartz with basalt up to 20 wt. % (CB-20) and sintering at 1150°C.

INTRODUCTION

Stoneware, a dense ceramic material, is commonly used for manufacturing floor and wall tiles. The characteristics of stoneware sintered products are low water absorption (< 0.5 % according to ISO 13006) with good physical and mechanical properties such as high hardness, abrasion resistance, and bending strength. Stoneware body ordinarily consists of a mixture of the main components including kaolin, ball clay, feldspar and quartz. Typically, stoneware compositions contain 30 - 40 % plastic components (kaolin and clay), 45-55 % fluxing agent (feldspar), and 5 - 20 % grog (quartz) [1-2]. Many researchers have studied alternative materials such as granite wastes, fly ash, pyrophyllite, and basalt rock for replacing clay-based ceramic components [3-8].

Also wollastonite, a CaO-rich mineral with needle-shaped crystals, has been used in ceramic production, including stoneware. In this context wollastonite acts as a fiber-reinforcement similar as in fiber composites. It improves the strength of ceramic green bodies and offers low firing temperature due to fluxing characteristics [9-11]. From this point of view, it is worthwhile investigating the idea of using another fiber material, basalt fiber, as an alternative raw material for clay-based ceramics. So far, however, there are only a few reports focusing on the application of basalt fibers in ceramic production [12]. Basalt fiber is an inorganic fiber extruded from melted basalt rock. The production of this fiber is similar to glass fiber, but it requires less energy and no additives, causing the low cost of production compared to glass or carbon fibers [12-13]. Generally, the main components of basalt are SiO₂ and Al₂O₃, with minor constituents including Fe₂O₃, CaO, MgO, Na₂O, TiO₂, and K₂O [14]. That means from the viewpoint of its chemical composition, basalt fiber contains several oxides found also in ceramic raw materials.

This work, basalt fibers are used for replacing some ceramic components such as quartz and potash feldspar in amounts of 10 - 25 wt. %. The mixtures are sintered at various temperatures between 1000 and 1200°C. The effect of basalt substitution on the physical and mechanical properties of the ceramics is discussed.

EXPERIMENTAL

Commercial clays, including kaolin (Amarin Ceramics Co., Ltd, Thailand) and ball clay (Compound Clay Co., Ltd, Thailand), potassium feldspar (Amarin Ceramics Co., Ltd, Thailand), and quartz (Cernic International Co., Ltd, Thailand) were used as raw materials for ceramic production. Basalt fiber used as an additional raw material came from a local basalt plant from Thailand (Siamfrit Co., Ltd, Thailand) (Figure 1). The chemical composition of these raw materials was analyzed by X-ray fluorescence (XRF). The ceramic compositions were prepared by mixing 50 % clay (25 % kaolin and 25 % ball clay), 25 % quartz and 25 % potassium feldspar. Both quartz and feldspar were replaced by basalt fiber in different amounts as shown in Table 1.
The powders were mixed in proper amounts by conventional ball milling with water for 24 h using alumina milling media. After milling, the slurry was dried at 100°C. The mixed powder then passed through a 100-mesh screen and, was uniaxially pressed at 31 MPa to form a bar-shaped specimen (3 × 4 × 30 mm). The green density of specimens was in the range of 1.5 - 1.6 g·cm⁻³. The samples were sintered in an electric furnace at five different temperatures (1000, 1050, 1100, 1150, and 1200°C) for 1 h with a heating rate of 5°C·min⁻¹. The density and porosity of sintered samples were determined using the Archimedes method. The linear shrinkage was measured by dimension calculation.

Table 2 presents the chemical compositions of the raw materials for ceramic production. The results showed that kaolin and ball clay mainly consisted of SiO₂ and Al₂O₃ with a small amount of CaO, MgO, Fe₂O₃, K₂O, etc. The quartz is 97.8 % pure SiO₂. Silica is used as a filler and stabilizer (grog) in ceramic materials [7, 15]. Feldspar as a fluxing agent mainly composed of SiO₂, Al₂O₃ and K₂O. Basalt fibers chiefly consist of SiO₂, Al₂O₃ and CaO. Other oxides present in relatively minor amounts include MgO, TiO₂ and Fe₂O₃. Although basalt fibers introduce a high amount of CaO and MgO into the mixture, they are still aluminosilicates, and thus it is not unreasonable to use them as a raw material for stoneware tile production.

Physical and mechanical properties

The physical and mechanical properties, including the mineralogy and microstructure were examined to assess the effect of basalts in ceramic compositions. Figure 2 presents the physical properties of ceramic (CB-0) and ceramic-basalt samples (CB-F25, CB-Q25, CB-10, and CB-20) sintered at 1000 to 1200°C. The linear shrinkage of ceramic (CB-0) increased with increasing firing temperature. The addition of basalt fiber could lower the shrinkage of ceramic especially with CB-10 and CB-20. In addition, the linear shrinkage of CB-10 and CB-20 significantly decreased, and the volume of samples consequently expanded at 1200°C. This result indicated that the excessive heat treatment of samples caused an overfiring effect [2, 6]. The presence of liquid phase is critical for densification.

Figure 2b shows the bulk densities of the sintered samples after sintering at different temperatures. In case of CB-F25 and CB-Q25, the density of the ceramic-basalt samples tended to increase slowly at low sintering temperature then sharply increased after 1100°C. On the other hand, the densification of the CB-10 and CB-20 increased with respect to the increase of sintering temperature up to 1150°C and then significantly decreased with further rise in temperature up to 1200°C.
due to overfiring of samples. This phenomenon resulted from the secondary fluxing agents such as CaO and MgO found in basalt components. These oxides may enhance or accelerate the densification by liquid phase formation in ceramic samples. However, increasing the temperature beyond the maximum densification of samples may cause overfiring effects and consequently reduced density [2, 6]. This is consistent with the reduced shrinkage and may be a consequence of the fact that melts with higher CaO and MgO contents do not wet the aluminosilicate surfaces. In extreme cases this may lead to swelling [16]. Comparing the basalt substitution in ceramic compositions, it was found that the partial replacement of both feldspar and quartz by basalt (CB-10, CB-20) showed superior densification than the entire replacement of feldspar or quartz by basalt (CB-F25, CB-Q25) as long as the CaO and MgO contents and the firing temperature is not too high. The CB-10 and CB-20 exhibited the maximum density of 2.48 and 2.40 g cm$^{-3}$ at a sintering temperature of 1150°C. These values are comparable to the density of typical porcelain-like body, 2.3 - 2.5 g cm$^{-3}$ [6].

Figure 2c shows the porosity of the ceramic-basalt samples as a function of temperature, where the porosity of the samples decreased as the sintering temperature increased. The reduction of porosity was significant after sintering at 1100°C for all samples. The lowest porosity was 0.03 - 0.08 % for CB-10 and CB-20 sintered at 1150°C. From these results, it can be concluded that the substitution of the basalt fibers in an appropriate amount enhanced the densification of ceramic products at a lower temperature compared to ceramic samples without basalt replacement.

Figure 3 displays the flexural strength of the ceramic-basalt samples as a function of the sintering temperature. The increase in temperature had a positive effect on the strength of ceramic samples. At lower temperatures (1000 - 1100°C), the strength values of ceramics made with basalt are higher than the basalt-free sample (CB-0). Interestingly, the strength of ceramics made with basalt sintered at 1100 - 1150°C (46 - 116 MPa) is even higher than the minimum strength values of ISO 13006 standards of ceramic tiles (35 MPa) [17].

---

**Figure 2.** Physical properties of the samples sintered at 1000 to 1200°C: a) linear shrinkage, b) bulk density, and c) porosity.

**Figure 3.** Flexural strength of the ceramic-basalt samples sintered at 1000 to 1200°C.
Utilization of basalt fibers as a raw material for clay ceramic production

Figure 4. XRD patterns of the ceramic compositions at 1150 and 1200°C: a) CB-0 and b) CB-20.

Figure 5. SEM micrographs of ceramic samples with and without basalts: a) CB-0; b) CB-20 sintered at 1150°C; c) CB-0; d) CB-20 sintered at 1200°C.
It was also found that the strengths of CB-20 at 1150°C are higher than basalt-free ceramics (CB-0) sintered at 1200°C. The CB-20 samples sintered at 1150°C exhibit the highest strength of 116 MPa. Unfortunately, the flexural strength of the CB-10 and CB-20 samples dropped rapidly at high firing temperature, 1200°C, which corresponds well to their low bulk densities as mentioned above. Increasing the temperature beyond maximum densification of samples led to overfiring. This phenomenon is responsible for the decrease in flexural strength at high temperature [2].

Phase analysis and microstructures

Figure 4 shows the XRD patterns of the crystalline phases of CB-0 and CB-20. The basalt-free ceramic sample (CB-0) consisted of quartz (SiO₂) and mullite (3Al₂O₃·2SiO₂). The crystalline phases detected in the ceramics made with basalt (CB-20) were anorthite (CaAl₂Si₂O₈), quartz (SiO₂) and mullite (3Al₂O₃·2SiO₂).

Figure 5 shows SEM micrographs of ceramic samples with and without basalt (CB-0 and CB-20) sintered at 1150 and 1200°C. In case of CB-0, the degree of densification increased with increasing temperature. In contrast, the ceramics made with basalt (CB-20) revealed more porosity at 1200°C due to overfiring as discussed earlier. The high porosity led to lower bulk density and flexural strength. Overall, basalt fiber can be added into clay-based ceramic compositions by replacing quartz and/or feldspar for ceramic productions in the production of tiles. The ceramic containing basalt fiber had a potential not only for enhancing the densification but also for decreasing the sintering temperature.

CONCLUSIONS

The substitution of basalt fibers (10 - 25 wt. %) for quartz and potash feldspar in different amounts affected both physical and mechanical properties of clay-based ceramic compositions. The partial replacement of both feldspar and quartz (CB-10, CB-20) by basalt showed higher density and strength than the complete replacement of feldspar or quartz (CB-F25, CB-Q25) by basalt. The substitution of the basalt fibers in appropriate amounts could enhance the densification and reduce sintering temperature of clay-based ceramics. In this study, ceramics made with basalt can be successfully sintered at a temperature of 1150°C. CB-20 exhibited the highest density and strength (2.40 g·cm⁻³ and 116 MPa, respectively). Therefore, it is possible to utilize basalt fibers as an alternative raw material in clay compositions for ceramic productions such as tiles.

Acknowledgements

This research was financially supported by the National Metal and Materials Technology Center, Thailand (Project No. MT-B-55-CER-07-293-I).

REFERENCES