

MECHANICAL PROPERTIES OF CARBON-CARBON COMPOSITE FOR IMPLANTS APPLICATIONS

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1. INTRODUCTION

New composite materials such as carbon-carbon composites for implants applications are moving rapidly out of the laboratory and into the hospital and clinic. C-C composites to be used in orthopedic in the form of intervertebral cages applied at lumbar spine injuries treatment have been investigated. A complex experimental project has been designed, first results of which being discussed in this paper.

on glass fibers considered as replacements and connections of long bones.

2. MATERIALS AND METHODS

2.1 Materials

Carbon-carbon composite samples are based on plain-woven cloth (Torayca carbon fibers T 800) and phenolic resin. Cured samples are carbonized at the heating rate of 50°C/hr up to 1000°C in nitrogen, see **Tab. I; Batch 1**. The preparation continues with three-step impregnation with phenolic resin and with repeated carbonization, see **Tab. I; Batch 1** and with graphitization at 2200°C in argon atmosphere, see **Tab. I; Batch 2, 3**. The finish step of manufacture is infiltration and covering with pyrolytic carbon in tumbling bed reactor, see **Tab. I; Batch 2, 3**. Our analysis of stress tested three different kinds of this composite with different final production technology applied. Not only a composite material exhibiting high strength values has been looking-for. Based on a complex analysis, the C-C composite exhibits a compromise between required both mechanical properties (a relatively sufficient strength value and a low modulus of elasticity, comparable with that of human bone), and biological properties (a sufficient porosity), which would be favourable for tissue and bone in growth, has been developed.

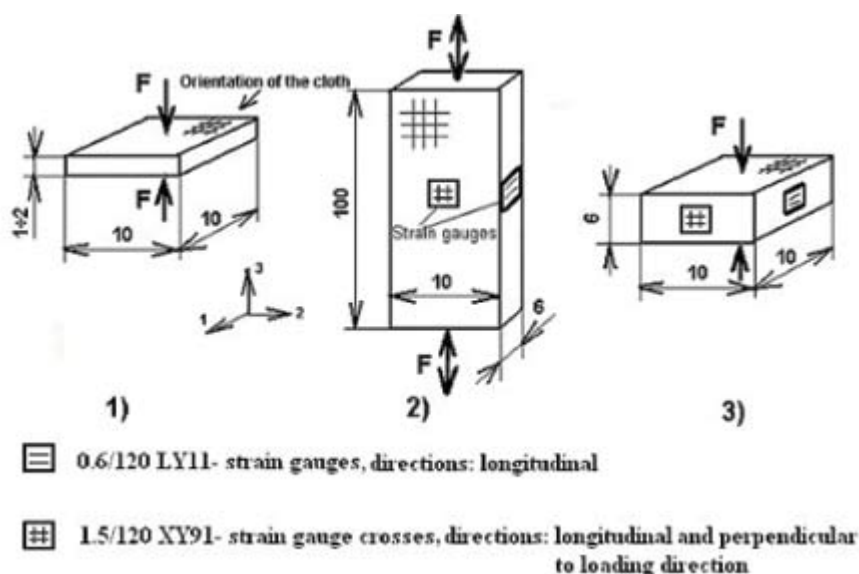


Fig. 1

Table I Batch

	A	Carbonized
1	B	Carbonized+1×impregnated
(see Fig.1)	C	Carbonized+3×impregnated
2	D	Carbonized+3×impregnated+graphited
(see Fig.1)	E	Carbonized+3×impregnated+graphited+PyC
3	F	Carbonized+3×impregnated+graphited
(see Fig.1)	G	Carbonized+3×impregnated+graphited+PyC

The **first research stage** dealt with testing of C/C-composite samples prepared as small specimens (**Fig.1** - scheme 1)). The experiments were carried out using the MTS Mini Bionix testing machine (MTS Systems Corp., USA). The testing machine jaw displacement (stroke) [mm], load [N], angle [deg] and torque [Nm] were measured in a configuration when the loading force was perpendicular to the composite laminae. It wasn't possible to use strain gauges, due to the small dimensions of this specimen and the mode of load application.

The **second and third research stages** have dealt with testing of samples, dimensions of which enabled to use strain gauges, **Fig.1**, while applying loading forces: in i) perpendicular - scheme **3**), and ii) parallel - scheme **2**), directions, respectively, to the composite laminae. More complex information about carbon-carbon composite has been obtained: E_1 and E_3 , respectively, Poisson's ratio μ_p , $\mu_{31}=\mu_{32}$, and stress limit values $\sigma_{1,3lim}$ both in tension and compression, provided that $\mu_{ij} = -\varepsilon_i / \varepsilon_j$. To ensure a full contact between the tested samples and the hydraulic jaws, special fixtures were manufactured combined with bone cement. Based on the experiences from the first measuring stage, a **basal loading mode**, chosen **for the second experimental stage** was as follows: a lower-rate loading (1000N, repeated 3x) and, after a 60s delay, the same lower-rate loading (3×). During all the six cycles, there was a maximum compressive loading force of 1 kN applied.

The **basal loading modes** were executed to determine mechanical characteristics of C-C composite samples made by the following technologies: i) **Batch 2, 3F**; ii) **Batch 2, 3G**.

Besides the basal loading mode, a complex loading mode was proposed, consisting in: i) four steps without interruption (2,3,4,5 kN); ii) five steps without interruption (6,7,8,9,10 kN); iii) the sample destruction test.

3. RESULTS AND DISCUSSION

The experiments presented in this paper have had a pilot character. They have been designed to provide mechanical characteristics of C-C composite to be applied in FEM models of intervertebral cages. The problem is complicated due to the fact that C-C composite examined has been simultaneously developed aiming to match two important properties: i) suitable mechanical characteristics, to serve as implants, on one hand, and ii) a sufficient porosity, to enable a quality bone ingrowth, on the other hand.

The **first test stage** was applied on a thin samples prepared in the following modes: i) **Batch 1A** ; ii) **Batch 1B**; iii) **Batch 1C**, that were loaded perpendicularly to their carbon fabric layers, which resulted into a rather carbon matrix loading, while the composite reinforcement played a little role. After obtaining load - displacement graphs, resulting stresses and strains were computed (by using specimens dimensions) and corresponding stress-strain graphs were drawn (see **Fig.2**).

Based on the linear part of the stress-strain graphs, corresponding moduli of elasticity E_3 in compression for the tested material types were assessed. Due to a lack of superfluous samples, which could have served for a proper microscope examination of polished sample sections in various loading stages, it has not been found out if the matrix has not been damaged at a certain

load level. From that reason contemporary interpretation of the results obtained is as follows: The first (concave) knee of the curves can be attributed to an interface contact creation between the sample and the jaw fixations and the second (convex) knee can be explained either as yielding or destruction onset of the matrix.

Notice: Nevertheless, there can be quite different interpretation: the matrix is being damaged from the very loading onset and the curves measured are due to a gradual contact increase of the parallel carbon fabric layers. These dilemmas may be solved only after all the experiments and examinations planned have been carried out.

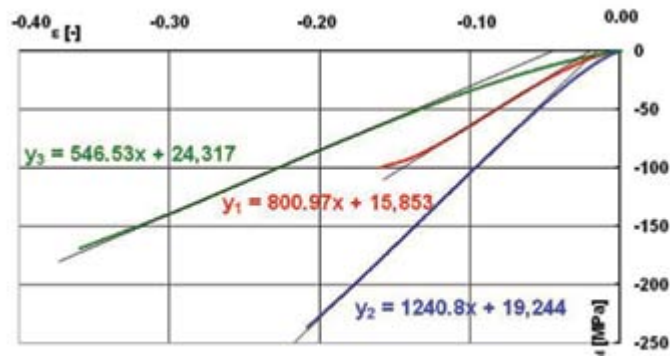


Fig. 2

Table II

Applications	Batch 1A	Batch 1B	Batch 1C
E_3 [Gpa]	0.801	0.55	1.24
σ_{3lim} [Mpa]	-72	-139	-201

Based on the linear part of the stress-strain graphs (**Fig. 2**), corresponding moduli of elasticity E_3 in compression for the tested material types were assessed (see **Tab. II**).

In the second test stage, C-C composite mechanical tests continued with the samples shown in **Fig. 1, 3**. Three samples have been tested, they have been prepared in the following modes: two samples – **Batch 3F** and one sample – **Batch 3G**. It is evident that results obtained from these tests serve only as preliminary information about mechanical behavior of the C-C composite developed. A basal mode (6 cycles, max. load of 1kN), where the first three cycles serve only for stabilization (in accordance with the Standard of the Aircraft Research Institute in Prague), was chosen for all the samples. For the first C+I+C+I+C+I+G sample, it was necessary to repeat all the six cycles with the same rate of max. applied load (1kN) since a too little response of the testing machine was adjusted. The **Batch 3G** sample was also tested by the basal mode (6 cycles, max. load of 1kN), **Fig. 2**.

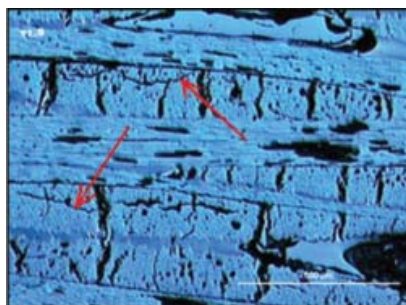


Fig. 2

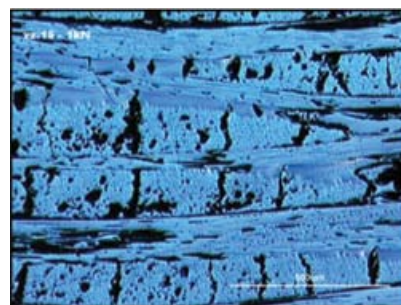


Fig. 3

These two samples were subjected to structural analyses (using the polished surface microscope scanning), **Fig. 3,4**. Meantime, the second **Batch 3F** sample was subjected to the complex lading mode.

After reading the scanning results of the first two samples (tested in 6 cycles, max. loaded 1 kN), some structural changes of the sample without PyC, **Fig. 3**, were found, different from those in the sample covered with PyC, **Fig. 4**, which confirmed a better behavior of the C-C composite with PyC and its better ability to be used in the developed intervertebral cages. Lower porosity of samples covered with PyC (i.e., a negative feature for its integration in the bone) can be improved by covering the C-C composite with the pHEMA (2-hydroxyethyl metacrylate), which stimulates the bone ingrowths into the composite.

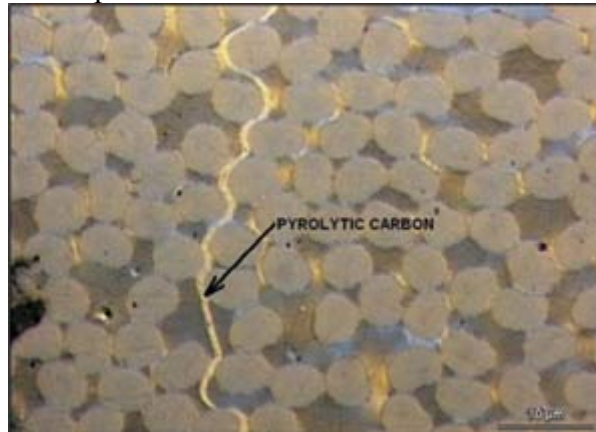


Fig. 5

Mechanical characteristics based on the second stage tests are listed in **Tab.III**. Although they cannot be used as statistically conclusive values (because of the small number of the tested samples) they basically show how different technologies (e.g., a comparison between samples covered or uncovered with PyC) influence their mechanical characteristics (see **Fig. 5**). (Based on the structural changes, the **Batch 3F** sample nonstandard mechanical properties shown in **Tab.III** can be explained). Recently tests continue with testing of samples **Batch 3 D, E** (loading force is parallel to the composite laminae, assessment of E_1)

Table III

Applications	Batch 3G	Batch 3F
E_3 [Gpa]	3.70	12.48
μ [-]	0.13	0.32

4. CONCLUSIONS

Mechanical compression tests of C-C composite samples, made by various technologies, served for choosing an optimum procedure yielding suitable mechanical characteristics for use in human lumbar spine injuries which preliminary resulted in the C-C composite infiltrated and covered with PyC. To obtain statistic informative values a sufficient number of samples to be mechanically tested has been prepared.

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PRVNÍ VÝSLEDKY VYSOKOTEPLTNÍCH MĚŘENÍ NA UNIVERZÁLNÍ TESTOVACÍ STROJ INSPEKT

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Přístroj Inspekt je již několik měsíců úspěšně využíván pro standardně užívané mechanické testy, především pro měření pevnosti C-C kompozitů v tříbodovém ohybu. Dále byly prováděny experimenty při vysokých teplotách na kompozitních materiálech s keramickými vlákny a sklokeramickou maticí. Při teplotách 1000°C až 1300 °C byl měřen Youngův modul pružnosti v konfiguraci čtyřbodového ohybu. Tento experiment byl prováděn při různých rychlostech deformace. Výsledky tohoto experimentu ukazují, že zvolená rychlost deformace má zřetelný vliv na měřený modul pružnosti. Je třeba poznamenat, že měřicí systém Maytec, detekující deformaci čtyřbodového ohybu ve středním poli nosníku, dává velmi spolehlivé výsledky. To bylo prokázáno srovnávacími měřeními s metodou rezonančních frekvencí a měřením materiálů se známými vlastnostmi při pokojových teplotách. Dalším vysokoteplotním experimentem, při kterém byl využit přístroj Inspekt bylo předběžné měření pevnosti v ohybu již výše zmíněných kompozitů s keramickými vlákny a sklokeramickou maticí. Na základě výsledků těchto měření bude možno plánovat optimální parametry objektivního experimentu, především počet vzorků a geometrii měřených těles.



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